# An Introduction to Wake Fields and Impedances

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# Abstract

The concepts of wake fields and impedance are introduced to describe the electromagnetic interaction of a bunch of charged particles with its environment in an particle accelerator. The various components of the environment are the vacuum chamber, cavities, bellows, dielectric-coated pipes, and other kinds of obstacles that the beam has to pass on its way through the accelerator. The wake fields can act back on the beam and lead to instabilities, which may limit the achievable current per bunch, the total current, or even both. Some typical examples are used to illustrate the wake function and its basic properties. Then wake fields in cavities and resonant structures are studied in detail. Finally, the frequency-domain view of the wake field or impedance is explained, and basic properties of the impedance are derived.

# Keywords

Wake field; impedance; modes in a cavity.

# 1 Introduction

A beam in an accelerator interacts with its vacuum chamber surroundings via electromagnetic fields. In this lecture the concept of wake fields is introduced to describe the electromagnetic interaction of a bunch of charged particles with its environment. The various components of the environment are the vacuum chamber, cavities, bellows, dielectric-coated pipes, and other kinds of obstacles the beam has to pass on its way through the accelerator. The wake fields can act back on the beam and lead to instabilities, which may limit the achievable current per bunch, the total current, or even both.

This lecture builds upon a previous lecture on wake fields and impedance given by T. Weiland about 25 years ago [1]. We recommend that the reader also consult the excellent textbooks [2–4] which cover the subject matter of this lecture.

We start with some typical examples from accelerator physics in which wake field effects are important.

Then, in Section 2, the concept of wake potential is formally introduced and multipole expansions are studied for structures with cylindrical symmetry. The Panofsky–Wenzel theorem, which links the longitudinal and transverse wake forces, is explained.

Section 3 is devoted to the analysis of wake fields due to resonant modes in a cavity. The fundamental theorem of beam loading is explained in detail. Finally, analytical results for a pillbox cavity are presented. The coupling of the beam to one mode of a cavity leads to the concept of the loss parameter.

In Section 4, the impedance is introduced as the Fourier transform of the wake potential. The properties of the wake functions (time-domain view) are translated to properties of the impedance (frequencydomain view).

# 1.1 Basic concepts

Consider a point charge q moving in free space at a velocity v close to the speed of light. The electromagnetic field is Lorentz-contracted into a thin disk perpendicular to the particle's direction of motion [5], which we choose to be the z-axis in a cylindrical coordinate system. The opening angle of the field

distribution is of the order of  $1/\gamma$ , where  $\gamma = (1 - (v/c)^2)^{-1/2}$ . The field distribution is shown in Fig. 1. Even for an electron beam with an energy of E = 10 MeV, the opening angle  $\phi$  is no greater than 50 mrad or 2.89°:

$$\phi = \frac{1}{\gamma} = \frac{0.511 \,\mathrm{MeV}}{E} = 2.89^{\circ}$$

 $(m_0 c^2 = 0.511 \,\mathrm{MeV}$  is the rest mass of the electron).

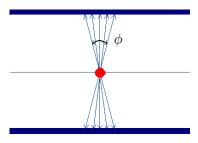


Fig. 1: Electromagnetic field carried by a relativistic point charge q

In the ultra-relativistic limit  $v \to c$  (or  $\gamma \to \infty$ ), the disk containing the field shrinks to a  $\delta$ -function distribution. The non-vanishing field components are

$$E_r = \frac{q}{2\pi \varepsilon_0 r} \,\delta(z - c t), \qquad H_\varphi = \frac{E_r}{Z_0} \quad \text{with } Z_0 = 377 \,\Omega.$$

Since the electric field E points strictly radially outward from the point charge, all field components are identically zero both ahead of and behind the point charge, and hence there are no forces on a test particle either preceding or following the charge q.

For v slightly less than c, this is not strictly true. However, if we look at some typical bunch charges and energies of high-energy accelerators and synchrotron light sources, as shown in Table 1, we will notice that the space charge force  $V_s = e/(4 \pi \epsilon_0 d^2 \gamma^2)$  (where d is the rms distance between two electrons in the bunch) scales with  $1/\gamma^2$ . It is then obvious that as a good approximation, any space charge effects can be neglected for the accelerators under consideration. Nevertheless, space charge effects are important in heavy ion or low-energy proton accelerators.

Machine	Charge (nC)	Energy (GeV)	$\gamma = (1 - (v/c)^2)^{-1/2}$
LHC	20	7000	7 500
LEP	100	60	195 700
PETRA III	20	6	11 700

Table 1: Typical bunch charges and energies of high-energy accelerators and synchrotron light sources [6–8]

In the next section we will restrict ourselves to the ultra-relativistic case ( $\gamma = \infty$ , v = c), so space charge effects are neglected.

# **1.2** Some simple examples

Consider some typical settings where electromagnetic fields occur behind a bunch with charge q moving with velocity c through a structure. A bunch moves through a cylindrical pipe along the z-axis. All electric field lines terminate transversely on surface charges on the wall of the pipe, assuming a perfectly

conducting wall. There will be no wake fields behind the charge. The situation is different, however, if the cross-section of the beam pipe changes. A step-out transition is shown in Fig. 2. All fields have been calculated using a numerical wake field solver from MAFIA or the CST studio suite [9-12]. Here

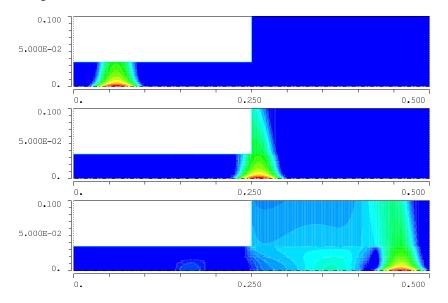


Fig. 2: Wake fields behind a bunch generated at a step-out transition from a small to a larger beam pipe

we have assumed that all pipe walls are perfect conductors. The wake field is generated because of the change in geometry. It should be noted that any beam pipe with finite conductivity, as well as flat beam pipes, can generate wake fields (resistive wall wake fields) [13]. Furthermore, a dielectric-coated pipe, which could be used as a travelling-wave acceleration section, will generate wake fields; see, for example, [14].

Another example is a cavity in a beam pipe; see Fig. 3. Again, a bunch is moving through a cylindrical pipe along the *z*-axis. Wake fields are generated because of geometrical changes in the pipe cross-section. In this respect the situation is similar to the previously considered case of a step-out transition. The main difference is that the bunch can excite modes in the cavity and therefore long-range wake fields, which can ring for a long time in the cavity (depending on the conductivity of the cavity wall).

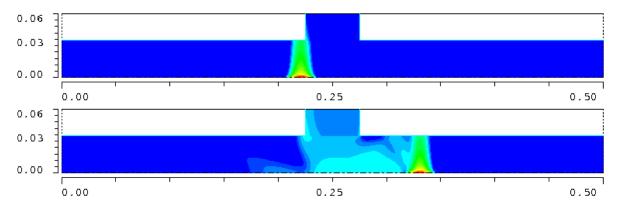


Fig. 3: Wake fields in a cavity

From these basic considerations we have learned that for electron accelerators the dominant wake forces are caused by geometrical changes along the beam pipe. Space charge effects are negligible for ultra-relativistic particles. Wake fields due to the resistive wall or dielectric coatings should always be checked in detail according to the specific situation.

# 2 Wake fields

#### 2.1 Wake fields in a resonant cavity with beam pipes

The examples above give us a qualitative understanding of wake fields and how they are generated. Before proceeding to mathematical descriptions in terms of wake potentials, let us take a closer look at the example considered in Section 1.

An ultra-relativistic point particle with charge  $q_1$  traverses a small cavity parallel to the z-axis, with offset  $(x_1, y_1)$ ; see Fig. 4. The electromagnetic force on any test charge  $q_2$  is given as a function of

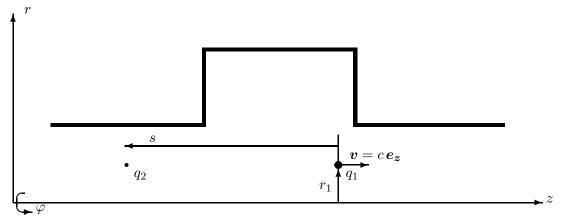


Fig. 4: An ultra-relativistic point particle with charge  $q_1$  traverses a small cavity parallel to the z-axis, followed by a test charge  $q_2$ 

space and time coordinates by the Lorentz equation

$$\boldsymbol{F}(\boldsymbol{r},t) = q_2 \big( \boldsymbol{E}(\boldsymbol{r},t) + \boldsymbol{v} \times \boldsymbol{B}(\boldsymbol{r},t) \big),$$

where E and B are the fields generated by  $q_1$ ; they are solutions of the Maxwell equations

$$\nabla \times \boldsymbol{B} = \mu_0 \boldsymbol{j} + \frac{1}{c^2} \frac{\partial}{\partial t} \boldsymbol{E}, \qquad \nabla \cdot \boldsymbol{B} = 0,$$
$$\nabla \times \boldsymbol{E} = -\frac{\partial}{\partial t} \boldsymbol{B}, \qquad \nabla \cdot \boldsymbol{E} = \frac{1}{\epsilon_0} \rho$$

and have to satisfy several boundary conditions.

In our case the charge and current distributions are

$$\rho(\mathbf{r},t) = q_1 \,\delta(x-x_1)\delta(y-y_1)\delta(z-ct),$$
$$\mathbf{j}(\mathbf{r},t) = c \,\mathbf{e_z} \,\rho(\mathbf{r},t).$$

After interaction of  $q_1$  with the cavity, there remain electromagnetic fields in the cavity. The source particle has lost energy to cavity modes and excited fields that propagate in the semi-infinite beam pipes.

Now consider a test charge  $q_2$  following  $q_1$  at a distance s with the same velocity  $v \approx c$  and with offset  $(x_2, y_2)$ . The Lorentz force is

$$F(x_1, y_1, x_2, y_2, s, t) = q_2 \big( E(x_2, y_2, z = ct - s, t) + c \, e_z \times B(x_2, y_2, z = ct - s, t) \big).$$

The change in momentum of the test charge can be calculated as the time-integrated Lorentz force,

$$\Delta \boldsymbol{p}(x_1, y_1, x_2, y_2, s) = \int \boldsymbol{F} \, \mathrm{d}t.$$

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This leads to the concept of wake functions.

The electromagnetic fields  $E_d$  and  $B_d$  and the Lorentz Force  $F_d$  of a distributed source  $\rho_d(r, t) = \eta(x_1 - \bar{x}_1, y_1 - \bar{y}_1)\lambda(z - ct)$  can be calculated either by integration over all source points,

$$\boldsymbol{F}_{\mathrm{d}}(\bar{x}_{1},\bar{y}_{1},x_{2},y_{2},s,t) = \int \boldsymbol{F}(x_{1},y_{1},x_{2},y_{2},s,t+z_{1}/c)\eta(x_{1}-\bar{x}_{1},y_{1}-\bar{y}_{1})\frac{\lambda(z_{1})}{q_{1}}\,\mathrm{d}x_{1}\,\mathrm{d}y_{1}\,\mathrm{d}z_{1},$$

or by solving the electromagnetic problem for the distributed source; here  $\lambda$  is the line charge density,  $\eta$  is the transverse distribution normalized to 1, and  $\bar{x}_1$  and  $\bar{y}_1$  describe a transverse shift of the center of the distribution. A calculation of the electric fields of a distributed source is shown in Fig. 5.

A fundamental difference between fields of point particles (with time dependency  $\delta(z - ct)$ ) and fields of distributed sources (with time dependency  $\lambda(z - ct)$ ) is that the frequency spectrum of point particles is not limited. In particular, long Gaussian bunches may stimulate only a few resonances (modes) in a cavity structure, or even none.

We can distinguish between the long-range regime of the wake, where the interaction between particles is driven by resonances, and the short-range regime, where the superposition of time-harmonic cavity fields is not sufficient to describe the effects. For instance, the fields in Fig. 2 are not determined by oscillations, while the fields in Fig. 5 will ring harmonically on one or several frequencies after the (source) bunch has left the domain.

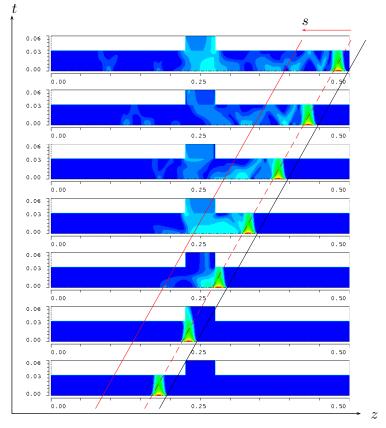


Fig. 5: Wake fields generated by a Gaussian bunch traversing a cavity

#### 2.2 Basic definitions

Consider a point charge  $q_1$  traversing a structure with offset  $(x_1, y_1)$  parallel to the z-axis at the speed of light (see Fig. 4). Then the *wake function* is defined as

$$\boldsymbol{w}(x_1, y_1, x_2, y_2, s) = \frac{1}{q_1} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \boldsymbol{E}(x_2, y_2, z, t) + c \, \boldsymbol{e}_z \times \boldsymbol{B}(x_2, y_2, z, t) \right]_{t = (s+z)/c}.$$

The distance s is measured from the source  $q_1$  in the opposite direction to v. The change in momentum of a test particle with charge  $q_2$  following behind at a distance s with offset  $(x_2, y_2)$  is given by

$$\Delta \boldsymbol{p} = \frac{1}{c} q_1 q_2 \boldsymbol{w}(s).$$

Since  $e_z \cdot (e_z \times B) = 0$ , the longitudinal component of the wake function is simply

$$w_{\parallel}(x_1, y_1, x_2, y_2, s) = \frac{1}{q_1} \int_{-\infty}^{\infty} \mathrm{d}z \, E_z(x_2, y_2, z, (s+z)/c).$$

Figure 6 shows the longitudinal component of the wake potential for the above example with the small cavity. The gray line represents the Gaussian charge distribution in the range from  $-5\sigma$  to  $10\sigma$ . Owing to transient wake field effects, the head of the bunch (left-hand side of the figure) is decelerated, while a test charge at a certain position behind the bunch will be accelerated.

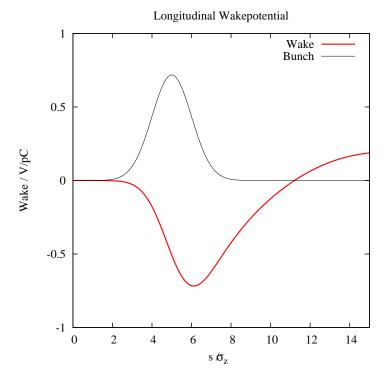


Fig. 6: Longitudinal wake potential

The notion of wakes, as presented above, is restricted to sources and test particles that travel at the velocity of light through a structure with semi-infinite input and output beam pipes. Therefore, for the integrals to converge, it is necessary that there be no length-independent forces in the pure beam pipes. This is the case for  $v \rightarrow c$  and perfect conductivity of the pipes. The concept of a wake per length,

$$\boldsymbol{w}'(x_1, y_1, x_2, y_2, s) = \frac{1}{q_1} \big[ \boldsymbol{E}_{\mathrm{p}}(x_2, y_2, -s, 0) + v \, \boldsymbol{e}_z \times \boldsymbol{B}_{\mathrm{p}}(x_2, y_2, -s, 0) \big],$$

is used to describe the effect in beam pipes 'p' of finite conductivity and/or velocity  $v \le c$ . Suppose that the input and output beam pipes have the same cross-section; then a generalized wake function

$$\boldsymbol{w}_{s}(x_{1}, y_{1}, x_{2}, y_{2}, s) = \frac{1}{q_{1}} \int_{-\infty}^{\infty} dz \left[ \boldsymbol{E}_{s}(x_{2}, y_{2}, z, t) + v \, \boldsymbol{e}_{z} \times \boldsymbol{B}_{s}(x_{2}, y_{2}, z, t) \right]_{t=(s+z)/v}$$

can be defined for the scattered fields  $E_s = E - E_p$  and  $B_s = B - B_p$ . If the conditions for the wake function are fulfilled (i.e. convergence of the integral), then the wake function equals the generalized wake function.

The wake potential is defined similarly to the wake function, but for a distributed source:

$$\boldsymbol{W}(\bar{x}_1, \bar{y}_1, x_2, y_2, s) = \frac{1}{q_1} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \boldsymbol{E}_{\mathrm{d}}(x_2, y_2, z, t) + c \, \boldsymbol{e}_z \times \boldsymbol{B}_{\mathrm{d}}(x_2, y_2, z, t) \right]_{t=(s+z)/c}$$
  
=  $\frac{1}{q_1 q_2} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \boldsymbol{F}_{\mathrm{d}}(\bar{x}_1, \bar{y}_1, x_2, y_2, z, t) \right]_{t=(s+z)/c}.$ 

It can be calculated from the wake function by the convolution

$$\boldsymbol{W}_{\mathrm{d}}(\bar{x}_{1}, \bar{y}_{1}, x_{2}, y_{2}, s) = \int \boldsymbol{w}(x_{1}, y_{1}, x_{2}, y_{2}, s + z_{1})\eta(x_{1} - \bar{x}_{1}, y_{1} - \bar{y}_{1})\frac{\lambda(z_{1})}{q_{1}}\,\mathrm{d}x_{1}\,\mathrm{d}y_{1}\,\mathrm{d}z_{1}.$$

Note that the *s*-coordinate measures in the negative *z*-direction while  $\lambda$  depends on the positive longitudinal coordinate. Usually numerical codes for computing wakes, such as ECHO, calculate electromagnetic fields for distributed sources and therefore wake potentials.

## 2.3 Some theory

# 2.3.1 The Panofsky–Wenzel theorem

We follow the arguments of A. Chao [2, 15] to introduce the Panofsky–Wenzel theorem [16]. Therefore we use the following different notation for the generalized wake function:

$$\boldsymbol{w}_{\mathrm{p}}(x_1, y_1, x_2, y_2, s) = \boldsymbol{w}_{\mathrm{p}}(x_1, y_1, \boldsymbol{r}_2),$$

with the observer vector  $\mathbf{r}_2 = x_2 \mathbf{e}_x + y_2 \mathbf{e}_y - s \mathbf{e}_z$ . We calculate curl  $\mathbf{w}_p$  with respect to the observer or the test particle:

$$\nabla_2 \times \boldsymbol{w}_{\mathrm{p}}(x_1, y_1, \boldsymbol{r}_2) = \nabla_2 \times \frac{v}{q_1} \int_{-\infty}^{\infty} \mathrm{d}t \left[ \boldsymbol{E}_{\mathrm{s}}(\boldsymbol{r}_2 + \boldsymbol{v}t, t) + \boldsymbol{v} \times \boldsymbol{B}_{\mathrm{s}}(\boldsymbol{r}_2 + \boldsymbol{v}t, t) \right].$$

Using curl  $\boldsymbol{E} = -\partial \boldsymbol{B} / \partial t$  gives

$$\nabla_{2} \times \boldsymbol{w}_{\mathrm{p}}(\boldsymbol{x}_{1}, \boldsymbol{y}_{1}, \boldsymbol{r}_{2}) = \frac{v}{q_{1}} \int_{-\infty}^{\infty} \mathrm{d}t \left[ -\frac{\partial}{\partial t} \boldsymbol{B}_{\mathrm{s}}(\dots, t) + \boldsymbol{v}(\nabla_{2}\boldsymbol{B}_{\mathrm{s}}(\dots, t)) - \boldsymbol{B}_{\mathrm{s}}(\dots, t)(\nabla_{2}\boldsymbol{v}) \right]$$
$$= \frac{v}{q_{1}} \int_{-\infty}^{\infty} \mathrm{d}t \left[ -\frac{\partial}{\partial t} - v\frac{\partial}{\partial z} \right] \boldsymbol{B}_{\mathrm{s}}(\boldsymbol{r}_{2} + \boldsymbol{v}t, t)$$
$$= \frac{v}{q_{1}} \int_{-\infty}^{\infty} \mathrm{d}t \left[ -\frac{\mathrm{d}}{\mathrm{d}t} \boldsymbol{B}_{\mathrm{s}}(\boldsymbol{r}_{2} + \boldsymbol{v}t, t) \right]$$
$$= -\frac{v}{q_{1}} \boldsymbol{B}_{\mathrm{s}}(\boldsymbol{r}_{2} + \boldsymbol{v}t, t) \Big|_{t=-\infty}^{t=\infty}.$$

As the scattered field is zero for negative infinite time and vanishes for positive infinite time and infinite distance from the scattering object, the wake is curl-free. The Panofsky–Wenzel theorem is then reformulated in our original notation as the set of equations

$$\frac{\partial}{\partial s}w_{\mathbf{p}x} = -\frac{\partial}{\partial x_2}w_{\mathbf{p}\parallel},$$

$$\frac{\partial}{\partial s} w_{\mathrm{p}y} = -\frac{\partial}{\partial y_2} w_{\mathrm{p}\parallel},$$
$$\frac{\partial}{\partial x_2} w_{\mathrm{p}y} = \frac{\partial}{\partial y_2} w_{\mathrm{p}x}.$$

Note that the Panofsky–Wenzel theorem holds for the generalized wake function ( $v \le c$ ) and for the wake function (v = c).

Integration of the transverse gradient of the longitudinal wake function yields the transverse wake potential

$$\boldsymbol{w}_{\perp}(x_1, y_1, x_2, y_2, s) = -\boldsymbol{\nabla}_{2\perp} \int_{-\infty}^{s} \mathrm{d}s' \, w_{\parallel}(x_1, y_1, x_2, y_2, s').$$

#### 2.3.2 Wake is harmonic with respect to observer offset

Now we calculate div w with respect to the observer. First, note that

$$\nabla_2 \cdot \boldsymbol{w}(x_1, y_1, \boldsymbol{r}_2) = \nabla_2 \cdot \frac{c}{q_1} \int_{-\infty}^{\infty} \mathrm{d}t \left[ \boldsymbol{E}(\boldsymbol{r}_2 + \boldsymbol{c}t, t) + \boldsymbol{c} \times \boldsymbol{B}(\boldsymbol{r}_2 + \boldsymbol{c}t, t) \right].$$

Using Maxwell's equations, div  $E = \rho/\varepsilon$  and curl  $B = \mu J + c^{-2} \partial E/\partial t$ , together with  $J = c\rho$  gives

$$\nabla_2 \cdot \boldsymbol{w}(x_1, y_1, \boldsymbol{r}_2) = \frac{c}{q_1} \int_{-\infty}^{\infty} \mathrm{d}t \left[ \nabla_2 \cdot \boldsymbol{E} + \boldsymbol{c}(\nabla_2 \times \boldsymbol{B}) \right]$$
$$= \frac{1}{q_1} \int_{-\infty}^{\infty} \mathrm{d}t \left[ -\frac{\partial}{\partial t} E_z(\boldsymbol{r}_2 + \boldsymbol{c}t, t) \right]$$
$$= -\frac{1}{q_1} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \frac{\partial}{\partial s} E_z(\boldsymbol{r}_2 + z\boldsymbol{e}_z, (z+s)/c) \right]$$
$$= -\frac{\partial}{\partial s} w_{\parallel}(x_1, y_1, x_2, y_2, s).$$

The term  $\partial w_{\parallel}/\partial s$  appears on both sides of the equation, so we can write

$$\frac{\partial w_x}{\partial x_2} + \frac{\partial w_y}{\partial y_2} = 0$$

With the Panofsky–Wenzel equations we find that the longitudinal wake is a harmonic function with respect to the transverse coordinates of the test particle:

$$\left(\frac{\partial^2}{\partial x_2^2} + \frac{\partial^2}{\partial y_2^2}\right) w_{\parallel} = -\frac{\partial}{\partial s} \left(\frac{\partial w_x}{\partial x_2} + \frac{\partial w_y}{\partial y_2}\right) = 0.$$

#### 2.3.3 Wake is harmonic with respect to source offset

The longitudinal wake is also a harmonic function with respect to the transverse coordinates of the source particle [17], i.e.  $L_1 w_{\parallel} = 0$  with  $L_1 = \partial^2 / \partial x_1^2 + \partial^2 / \partial y_1^2$ . To prove this, we have to calculate  $\tilde{E}_z = L_1 E_z$ , which is equivalent to the solution of the field problem for the source  $\tilde{\rho} = L_1 \rho$ . The source  $\rho$  is the point particle  $q_1$  travelling at the speed of light along  $(x_1, y_1, z = ct)$ . It gives rise to the electromagnetic fields

$$\begin{aligned} \boldsymbol{E}_{\mathrm{f}} &= q_1 \frac{\delta(z-ct)}{2\pi\varepsilon} \frac{(x-x_1)\boldsymbol{e}_x + (y-y_1)\boldsymbol{e}_y}{(x-x_1)^2 + (y-y_1)^2},\\ \boldsymbol{B}_{\mathrm{f}} &= c^{-1}\boldsymbol{e}_z \times \boldsymbol{E}_{\mathrm{f}} \end{aligned}$$

in free space. The fields  $\tilde{E} = L_1 E_f$  and  $\tilde{B} = L_1 B_f$  are caused by the source  $\tilde{\rho} = L_1 \rho$ . These fields are zero for all points with  $(x, y) \neq (x_1, y_1)$ , as

$$\left(\frac{\partial^2}{\partial x_1^2} + \frac{\partial^2}{\partial y_1^2}\right)\frac{(x-x_1)\boldsymbol{e}_x + (y-y_1)\boldsymbol{e}_y}{(x-x_1)^2 + (y-y_1)^2} = \mathbf{0}.$$

Obviously  $\tilde{E}$  and  $\tilde{B}$  satisfy any linear boundary condition for any geometry, provided that the boundary does not intersect the trajectory  $(x_1, y_1, z = ct)$ . Therefore these fields are also solutions to the bounded wake problem, and all components of w are harmonic with respect to  $(x_1, y_1)$ , since

$$\left(\frac{\partial^2}{\partial x_1^2} + \frac{\partial^2}{\partial y_1^2}\right) \boldsymbol{w} = \frac{c}{q_1} \int_{-\infty}^{\infty} \mathrm{d}t \left[\tilde{\boldsymbol{E}} + \boldsymbol{c} \times \tilde{\boldsymbol{B}}\right] = \boldsymbol{0}.$$

This information will help us to evaluate the r-dependence of the wake function in cylindrical symmetric structures in the next subsection, and it will enable us to efficiently calculate the wake function in fully 3D structures.

## 2.3.4 Restrictions

The Panofsky–Wenzel theorem is applicable if the input and output beam pipes have the same crosssection. The longitudinal wake is harmonic if the trajectories  $(x_1, y_1, ct)$  and  $(x_2, y_2, ct)$  do not intersect with the boundary.

#### 2.4 Wake function in cylindrically symmetric structures

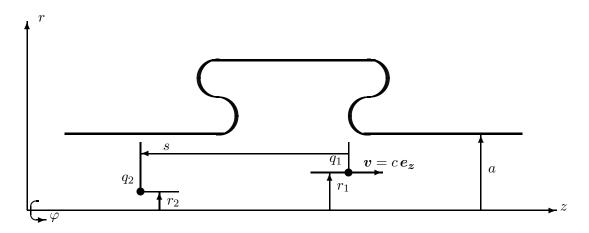


Fig. 7: A bunch with total charge  $q_1$  traversing a cavity with offset  $r_1$ , followed by a test charge  $q_2$  with offset  $r_2$ 

Consider now a cylindrically symmetric acceleration cavity with side tubes of radius a (see Fig. 7). The particular shape in the region r > a is of no importance for the following investigations. Two charges pass through the structure from left to right with the speed of light:  $q_1$  at a radius of  $r_1$  and  $q_2$  at a radius of  $r_2$ . We wish to find an expression for the net change in momentum,  $\Delta p(r_1, \varphi_1, r_2, \varphi_2, s)$ , experienced by  $q_2$  due to the wake fields generated by  $q_1$ . In the following we write the wake function and potential in polar coordinates. Let us start with the case of  $\varphi_1 = 0$ :

$$\Delta p_z(r_1, 0, r_2, \varphi_2, s) = q_1 q_2 w_{\parallel}(r_1, 0, r_2, \varphi_2, s).$$

The wake function can be expanded in a multipole series

$$w_{\parallel}(r_1, 0, r_2, \varphi_2, s) = \operatorname{Re}\left\{\sum_{m=-\infty}^{\infty} \exp(\operatorname{i} m \varphi_2) G_m(r_1, r_2, s)\right\}.$$

Since  $w_{\parallel}$  is a harmonic function in  $(r_2, \varphi_2)$ , we have

$$L_2 w_{\parallel}(r_1, 0, r_2, \varphi_2, s) = \left(\frac{1}{r_2} \frac{\partial}{\partial r_2} r_2 \frac{\partial}{\partial r_2} + \frac{1}{r^2} \frac{\partial^2}{\partial \varphi_2^2}\right) w_{\parallel}(r_1, 0, r_2, \varphi_2, s)$$
  
=  $\operatorname{Re} \left\{ \sum_{m=-\infty}^{\infty} \exp(\operatorname{i} m \varphi_2) \left(\frac{1}{r_2} \frac{\partial}{\partial r_2} r_2 \frac{\partial}{\partial r_2} - \frac{m^2}{r_2^2}\right) G_m(r_1, r_2, s) \right\}$   
= 0,

where  $L_2$  is the transverse Laplace operator with respect to the offset of the test particle. So, for all m, the expansion functions  $G_m(r_1, r_2, s)$  have to satisfy the Poisson equation

$$\frac{1}{r_2}\frac{\partial}{\partial r_2}\left(r_2\frac{\partial}{\partial r_2}G_m(r_1, r_2, s)\right) - \frac{m^2}{r_2^2}G_m(r_1, r_2, s) = 0.$$

The solutions are

$$G_0(r_1, r_2, s) = U_0(r_1, s) + V_0(r_1, s) \ln r_2,$$
  

$$G_m(r_1, r_2, s) = U_m(r_1, s) r_2^m + V_m(r_1, s) r_2^{-m} \quad \text{for } m > 0.$$

Keeping only the solutions which are regular at the origin  $(r_2 = 0)$ , the longitudinal wake potential can be written as

$$w_{\parallel}(r_1, 0, r_2, \varphi_2, s) = \sum_{m=0}^{\infty} r_2^m U_m(r_1, s) \cos m\varphi_2,$$

with expansion functions  $U_m(r_1, s)$  that depend on the details of the given cavity geometry.

By azimuthal symmetry, the dependence on  $\varphi_1$  is  $w_{\parallel}(r_1, \varphi_1, r_2, \varphi_2, s) = w_{\parallel}(r_1, 0, r_2, \varphi_2 - \varphi_2, s)$ , as longitudinal fields depend only on the relative azimuthal angle of the observer with respect to the source. Using the fact that  $w_{\parallel}$  is also a harmonic function in  $(r_1, \varphi_1)$ , we find with the same arguments as before that  $U_m(r_1, s)$  can be factorized as  $r_1^m w_m(s)$ .

It follows that for the general case of a charge  $q_1$  at  $(r_1, \varphi_1)$  generating fields that act on a second charge  $q_2$  at  $(r_2, \varphi_2)$ , the *longitudinal wake function* is given by

$$w_{\parallel}(r_1,\varphi_1,r_2,\varphi_2,s) = \sum_{m=0}^{\infty} r_1^m r_2^m w_m(s) \cos m(\varphi_2 - \varphi_1).$$

The transverse wake function is, by the Panofsky-Wenzel theorem,

$$\boldsymbol{w}_{\perp}(r_{1},\varphi_{1},r_{2},\varphi_{2},s) = -\left(\boldsymbol{e_{r}}\frac{\partial}{\partial r_{2}} + \boldsymbol{e_{\varphi}}\frac{1}{r_{2}}\frac{\partial}{\partial \varphi_{2}}\right)\int_{-\infty}^{s} \mathrm{d}s' \, w_{\parallel}(r_{1},\varphi_{1},r_{2},\varphi_{2},s')$$
$$= \sum_{m=0}^{\infty} \left\{-\boldsymbol{e_{r}} \, m \, r_{1}^{m} \, r_{2}^{m-1} \int_{-\infty}^{s} \mathrm{d}s' \, w_{m}(s') \, \cos m(\varphi_{2}-\varphi_{1})\right.$$
$$\left. + \boldsymbol{e_{\varphi}} \, m \, r_{1}^{m} \, r_{2}^{m-1} \int_{-\infty}^{s} \mathrm{d}s' \, w_{m}(s') \, \sin m(\varphi_{2}-\varphi_{1})\right\}$$

Each azimuthal order is fully characterized by a scalar function  $w_m(s)$ . This function can be calculated by solving Maxwell's equations for the given geometry and any choice of  $(r_1, \varphi_1, r_2, \varphi_2)$ , yielding

$$w_m(s) = \frac{\int_{-\infty}^{\infty} dz \, E_{zm}(r_2, \varphi_2, z, (z+s)/c))}{r_1^m \, r_2^m \, \cos m(\varphi_2 - \varphi_1)}.$$

# AN INTRODUCTION TO WAKE FIELDS AND IMPEDANCES

A particular choice of  $r_2$  can be used to avoid the infinite integration range: since  $E_z$  vanishes at the metallic tube boundary, only the cavity gap contributes to the integral. The integration range is reduced to the cavity gap by setting  $r_2$  to the radius of the beam tube. This trick is possible if no obstacle intersects with the infinite cylindrical beam pipe.

This type of wake integration is utilized by computer codes such as ECHO [18, 19] for bunches of finite length. Wake potentials can be calculated by such programs in the time domain, but wake functions (of point sources) need asymptotic considerations; see [20].

It should be mentioned that in many practical cases, due to the  $(r/a)^m$  dependence, the longitudinal wake is dominated by the monopole term and the transverse wakes by the dipole term:

$$w_{\parallel}(r_1,\varphi_1,r_2,\varphi_2,s) = w_0(s),$$
  
$$w_{\perp}(r_1,\varphi_1,r_2,\varphi_2,s) = r_1 \int_{-\infty}^s \mathrm{d}s' \, w_1(s') \left[ -\boldsymbol{e_r} \, \cos(\varphi_2 - \varphi_1) + \boldsymbol{e_{\varphi}} \, \sin(\varphi_2 - \varphi_1) \right].$$

## 2.5 Fully 3D structures

While for cylindrical symmetric structures the dependence of the wake on transverse coordinates is explicitly known and can be used to reduce the integration range and domain of the field calculation, more general structures require us to use the harmonic property of the wake for a beam tube of arbitrary shape. The simple 3D cavity in Fig. 8, with a beam tube of square cross-section, is used to demonstrate this. We suppress the dependence of the wake function (or potential) on the offset of the source and write simply  $\tilde{W}_{\parallel}(x, y, s) = W_{\parallel}(x_1, y_1, x, y, s)$ . This function is harmonic in the observer offset,

$$\boldsymbol{\nabla}_{\perp}^2 W_{\parallel}(x,y,s) = 0.$$

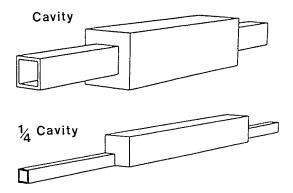
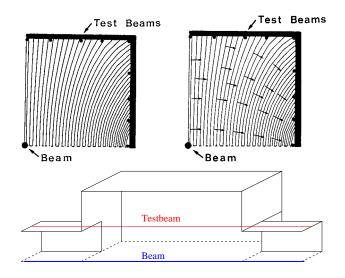


Fig. 8: A 3D cavity structure with two symmetry planes (top) and a quarter of the structure (bottom)

For points x and y on the surface of the beam tube, we can calculate the wake by a finite-range integration through the cavity gap, as shown in Fig. 9. If we know  $\tilde{W}$  for all surface points, we can calculate the wake for any point inside the tube by numerical solution of the boundary value problem. Therefore a 2D Poisson problem has to be solved. In our example, with two transverse symmetries, only a quarter of the structure needs to be considered to calculate the wake of a source in the center.

The transverse wake potential can be calculated from the longitudinal one using the Panofsky– Wenzel theorem. The transverse gradient of the longitudinal wake potential in a beam tube is also indicated in Fig. 9.



**Fig. 9:** Illustration of the indirect test beam method. The upper pictures show lines of constant longitudinal wake potential and the gradient of the longitudinal wake potential; an integration gives the transverse wake potential according to the Panofsky–Wenzel theorem. The lower diagram depicts the paths of the beam and the test beam.

## 3 Cavities, resonant structures and eigenmodes

#### 3.1 Eigenmodes

Many structures in an accelerator environment can be considered as a hollow space with semi-infinite beam pipes on both sides. Usually this vacuum volume is bounded by metal surfaces with high conductivity. As a good approximation, the cavity walls can be treated as perfect electric conducting (PEC) boundaries, and sometimes the beam pipes are even neglected so that the volume is closed.

Electromagnetic fields with frequencies below the lowest cutoff frequency of the beam pipes are trapped in the volume, and the fields oscillate at discrete frequencies:

$$\boldsymbol{E}(\boldsymbol{r},t) = \sum_{\nu} \hat{A}_{\nu} \hat{\boldsymbol{E}}_{\nu}(\boldsymbol{r}) \cos(\hat{\omega}_{\nu}t + \hat{\varphi}_{\nu}),$$
$$\boldsymbol{B}(\boldsymbol{r},t) = \sum_{\nu} \hat{A}_{\nu} \hat{\boldsymbol{B}}_{\nu}(\boldsymbol{r}) \sin(\hat{\omega}_{\nu}t + \hat{\varphi}_{\nu}).$$

These oscillations are called eigenmodes or cavity modes. They are characterized by their field patterns  $\hat{E}_{\nu}(\mathbf{r})$  and  $\hat{B}_{\nu}(\mathbf{r})$  and their eigenfrequencies  $\hat{\omega}_{\nu}$ . The modes may ring with any amplitude  $\hat{A}_{\nu}$  and phase  $\hat{\varphi}_{\nu}$ , and the amplitude normalization of the eigenfields is arbitrary. Such modes are called standing-wave modes, as the electric and magnetic fields ring at all spatial points with the same phase, but the electric field is phase-shifted by 90° relative to the magnetic field. For simplicity, in the following we omit the mode index  $\nu$  but indicate all indexable (mode-specific) quantities with a hat. We will introduce further mode-specific quantities, such as the quality  $\hat{Q}$ , the modal longitudinal loss parameter  $\hat{k}$ , and the mode energy

$$\hat{\mathcal{W}} = \frac{1}{2} \int \varepsilon \hat{E}^2 \, \mathrm{d}V = \frac{1}{2} \int \mu^{-1} \hat{B}^2 \, \mathrm{d}V$$

which depends on the arbitrary amplitude normalization. The total electromagnetic field energy of all the modes is<sup>1</sup>

$$\mathcal{W} = \frac{1}{2} \int \varepsilon E(\mathbf{r}, \mathbf{t})^2 \, \mathrm{d}V + \frac{1}{2} \int \mu^{-1} B(\mathbf{r}, \mathbf{t})^2 \, \mathrm{d}V = \sum |\hat{A}|^2 \, \hat{\mathcal{W}}.$$

<sup>&</sup>lt;sup>1</sup>The field energy of a particular mode does not depend on the stimulation of other modes, as the mode fields are orthogonal to each other; see Appendix A.

# AN INTRODUCTION TO WAKE FIELDS AND IMPEDANCES

Eigenmodes can be computed with electromagnetic field solvers such as those in [9, 10]; see also Fig. 10. Usually closed volumes are considered, which are completely surrounded by PEC or perfect magnetic conducting (PMC) surfaces. As the mode field in beam pipes decays exponentially, even open problems (involving infinitely long pipes) can be handled with such programs, by using a perfectly conducting boundary after a sufficiently long piece of pipe.

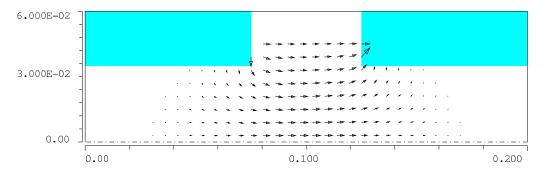


Fig. 10: Electric field of a mode in a rotationally symmetric cavity with beam pipes

In structures with symmetries (e.g. rotational symmetry), eigenmodes and beam-pipe modes of the same symmetry condition are coupled. Therefore the lowest cutoff frequency for a particular symmetry defines the highest possible eigenfrequency for the corresponding eigenmodes. For instance, monopole modes may have resonance frequencies that are above the lowest dipole mode cutoff frequency, which is lower than the lowest monopole mode cutoff frequency. Beyond that, there can exist quasi-trapped modes above the lowest cutoff frequency that have very weak coupling to the pipes. The energy flow (per period) of such fields into the beam pipes may be comparable to the energy loss (per period) of non-trapped modes to non-perfectly conducting metallic boundaries.

#### 3.2 Excitation of eigenmodes and the per-mode loss parameter

We consider a cavity of length<sup>2</sup> L and a bunch with charge  $q_1$ , offset  $(x_1, y_1)$  and velocity c, which enters the cavity at time t = 0. The electromagnetic fields after the charge has left the cavity, namely

$$\begin{split} \boldsymbol{E}(\boldsymbol{r},t > L/c) &= \sum \operatorname{Re} \{ \hat{A} \hat{\boldsymbol{E}}(\boldsymbol{r}) \exp(\mathrm{i}\,\hat{\omega}t) \} + \boldsymbol{E}_{\mathrm{r}}(\boldsymbol{r},t), \\ \boldsymbol{B}(\boldsymbol{r},t > L/c) &= \sum \operatorname{Im} \{ \hat{A} \hat{\boldsymbol{B}}(\boldsymbol{r}) \exp(\mathrm{i}\,\hat{\omega}t) \} + \boldsymbol{B}_{\mathrm{r}}(\boldsymbol{r},t), \end{split}$$

can be split into eigenfields and a residual part,  $E_r$  or  $B_r$ . The long-range interaction between bunches or particles is essentially driven by the modal part, as the residual fields decay or are not stimulated resonantly. The complex mode amplitudes are proportional to the source charge and depend on the source offset. Hence they can be expressed as  $\hat{A} = q_1 \hat{f}(x_1, y_1)$ .

Suppose that a small test charge  $\delta q$  follows the source particle on the same trajectory at a distance of s > 0. It induces the additional amplitude  $\delta \hat{A} = \delta q \exp(-i\hat{\omega}s/c)\hat{f}(x_1, y_1)$ . Therefore the energy of the modes is increased by

$$\begin{split} \delta \mathcal{W}_{\text{modes}} &= \sum \left( |\hat{A} + \delta \hat{A}|^2 - |\hat{A}|^2 \right) \hat{\mathcal{W}} \\ &\approx \sum 2 \operatorname{Re} \left\{ \hat{A} \delta \hat{A}^* \right\} \hat{\mathcal{W}} \\ &\approx 2q_1 \delta q \sum |\hat{f}(x_1, y_1)|^2 \operatorname{Re} \left\{ \exp(\mathrm{i}\,\hat{\omega}s/c) \right\} \hat{\mathcal{W}}. \end{split}$$

<sup>&</sup>lt;sup>2</sup>The relevant length is not exactly the length of the cavity, but rather the length with non-zero field of the modes. For open structures, with beam pipes, this length is in principle infinite, but for practical considerations the field has decayed sufficiently after a pipe length of a few times the widest dimension of the cross-section.

On the other hand, the test particle gains kinetic energy

$$\delta \mathcal{W}_{\mathbf{k}} = \int_{-\infty}^{\infty} \delta q \, E_z(x_1, y_1, z - s, z/c) \, \mathrm{d}z$$
$$= q_1 \delta q \sum \operatorname{Re} \left\{ \hat{f}(x_1, y_1) \int_{-\infty}^{\infty} \hat{E}_z(x_1, y_1, z) \exp(\mathrm{i}\,\hat{\omega}(z+s)/c) \, \mathrm{d}z \right\} + \cdots$$

The sum of the field energy and the kinetic energy is conserved, if terms with the same oscillation frequency  $\exp(i\hat{\omega}s/c)$  cancel:

$$2|\hat{f}(x_1,y_1)|^2 \hat{\mathcal{W}} + \hat{f}(x_1,y_1) \int_{-\infty}^{\infty} \hat{E}_z(x_1,y_1,z) \exp(\mathrm{i}\,\hat{\omega}(z)/c)\,\mathrm{d}z = 0.$$

This is satisfied with  $\hat{f}(x_1, y_1) = -\hat{v}^*(x_1, y_1)/\sqrt{\hat{\mathcal{W}}}$  and the normalized mode voltages

$$\hat{v}(x,y) = \frac{1}{2\sqrt{\hat{\mathcal{W}}}} \int_{-\infty}^{\infty} \hat{E}_z(x,y,z) \exp(\mathrm{i}\,\hat{\omega}z/c)\,\mathrm{d}z,$$

which do not depend on the arbitrary normalization mode fields.

The amplitude excited by the charge  $q_1$  is

$$\hat{A} = q_1 \hat{f}(x_1, y_1) = -q_1 \hat{v}^*(x_1, y_1) / \sqrt{\hat{\mathcal{W}}},$$

and the energy of all modes is

$$\mathcal{W}_{\text{EM,modes}} = \sum |\hat{A}|^2 \hat{W} = q_1^2 \sum \hat{k},$$

with the per-mode loss parameter

$$\hat{k} = |\hat{v}(x_1, y_1)|^2 = \frac{1}{4\hat{\mathcal{W}}} \left| \int_{-\infty}^{\infty} \hat{E}_z(x_1, y_1, z) \exp(\mathrm{i}\,\hat{\omega}(z)/c)\,\mathrm{d}z \right|^2.$$

The excitation of mode amplitudes depends linearly on the source distribution: another particle with charge  $q_2$  and offset  $(x_2, y_2)$  at a distance s gives rise to the additional amplitude

$$\hat{A} = -q_2 \hat{v}^*(x_2, y_2) \exp(-\mathrm{i}\,\hat{\omega}s/c) / \sqrt{\hat{\mathcal{W}}} \,,$$

with phase shift  $-\hat{\omega}s/c$  due to the time shift s/c. Therefore it is possible to calculate the mode excitation for arbitrary charge distributions; for example, for a one-dimensional bunch with offset  $(x_1, y_1)$  and line charge density  $\lambda(z, t) = \lambda(z - ct)$ ,

$$\hat{A} = \hat{v}^*(x_1, y_1) \int \lambda(-s) \exp(-\mathrm{i}\,\hat{\omega}s/c)\,\mathrm{d}s.$$

In particular, a Gaussian bunch with charge  $q_1$  and rms length  $\sigma$  excites the amplitudes  $\hat{A} = q_1 \hat{v}^*(x_1, y_1) \exp(-(\hat{\omega}\sigma/c)^2/2)$ . We introduce the shape-dependent per-mode loss parameter

$$\hat{k}_{\sigma} = \hat{k} \exp(-(\hat{\omega}\sigma/c)^2).$$

The electromagnetic field energy of all modes, after such a bunch has traversed the cavity, is

$$\mathcal{W}_{\text{EM,modes},\sigma} = \sum |\hat{A}|^2 \hat{\mathcal{W}} = q_1^2 \sum \hat{k}_{\sigma}.$$

#### 3.3 Contribution of eigenmodes to the wake function

After the source particle has traversed the cavity, the electromagnetic fields are

$$\begin{aligned} \boldsymbol{E}(\boldsymbol{r},t > L/c) &= q_1 \sum \operatorname{Re} \left\{ -\hat{v}^*(x_1,y_1) \hat{\mathcal{W}}^{-1/2} \hat{\boldsymbol{E}}(\boldsymbol{r}) \exp(\mathrm{i}\,\hat{\omega}t) \right\} + \boldsymbol{E}_{\mathrm{r}}(\boldsymbol{r},t), \\ \boldsymbol{B}(\boldsymbol{r},t > L/c) &= q_1 \sum \operatorname{Im} \left\{ -\hat{v}^*(x_1,y_1) \hat{\mathcal{W}}^{-1/2} \hat{\boldsymbol{B}}(\boldsymbol{r}) \exp(\mathrm{i}\,\hat{\omega}t) \right\} + \boldsymbol{B}_{\mathrm{r}}(\boldsymbol{r},t), \end{aligned}$$

Therefore the momentum of a test charge  $q_2$  at a distance s > L behind the source, with offset  $(x_2, y_2)$ and velocity c, is changed by

$$\Delta \boldsymbol{p} = \frac{q_1 q_2}{c} \sum \operatorname{Re} \left\{ -\hat{v}^*(x_1, y_1) \hat{\mathcal{W}}^{-1/2} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \left( \hat{\boldsymbol{E}} - \mathrm{i}\,\boldsymbol{c} \times \hat{\boldsymbol{B}} \right) \exp(\mathrm{i}\,\hat{\omega}(z+s)/c) \right] \right\} + \Delta \boldsymbol{p}_{\mathrm{r}},$$

where the term  $\Delta p_r$  stands for the contribution of the residual fields. Likewise, we can split the wake into modal and residual parts:

$$\boldsymbol{w}(x_1, y_1, x_2, y_2, s > L) = \frac{c\Delta \boldsymbol{p}}{q_1 q_2} = \sum \hat{\boldsymbol{w}}(x_1, y_1, x_2, y_2, s) + \boldsymbol{w}_{\mathrm{r}}(x_1, y_1, x_2, y_2, s),$$

where

$$\hat{\boldsymbol{w}}(x_1, y_1, x_2, y_2, s > L) = -2 \operatorname{Re} \{ \hat{v}^*(x_1, y_1) \hat{\boldsymbol{v}}(x_2, y_2) \exp(\mathrm{i}\,\hat{\omega}s/c) \},\$$

with the normalized vectorial voltages

$$\hat{\boldsymbol{v}}(x,y) = \frac{1}{2\sqrt{\hat{\mathcal{W}}}} \int_{-\infty}^{\infty} \mathrm{d}z \left[ \left( \hat{\boldsymbol{E}}(x,y,z) - \mathrm{i}\,\boldsymbol{c} \times \hat{\boldsymbol{B}}(x,y,z) \right) \exp(\mathrm{i}\,\hat{\omega}z/c) \right].$$

## 3.4 Causality and the fundamental theorem of beam loading

Consider two point particles with charges and coordinates  $q_1, x_1, y_1, z_1 = ct$  and  $q_2, x_2, y_2, z_2 = ct - s$ . The distance parameter s may be positive or negative. The electromagnetic fields are caused by both particles together. Therefore the integrated longitudinal fields observed by the particles are

$$V_{1} = \int E_{z}(x_{1}, y_{1}, z_{1}, t) dz = q_{1}w_{\parallel}(x_{1}, y_{1}, x_{1}, y_{1}, 0) + q_{2}w_{\parallel}(x_{2}, y_{2}, x_{1}, y_{1}, -s),$$
  

$$V_{2} = \int E_{z}(x_{2}, y_{2}, z_{2}, t) dz = q_{1}w_{\parallel}(x_{1}, y_{1}, x_{2}, y_{2}, s) + q_{2}w_{\parallel}(x_{2}, y_{2}, x_{2}, y_{2}, 0).$$

The gain of electromagnetic field energy,  $\Delta W_{\rm EM} = -q_1 V_1 - q_2 V_2$ , is always positive, as the interaction volume is initially field-free; it is

$$\begin{aligned} \Delta \mathcal{W}_{\text{EM,total}} &= -q_1^2 w_{\parallel}(x_1, y_1, x_1, y_1, 0) \\ &\quad -q_2^2 w_{\parallel}(x_2, y_2, x_2, y_2, 0) \\ &\quad -q_1 q_2 \Big( w_{\parallel}(x_1, y_1, x_2, y_2, s) + w_{\parallel}(x_2, y_2, x_1, y_1, -s) \Big). \end{aligned}$$

It is natural to write the electromagnetic field energy in terms of the per-mode and residual wake functions,

$$\begin{split} \Delta \mathcal{W}_{\text{EM,total}} &= -q_1^2 \sum \hat{w}_{\parallel}(x_1, y_1, x_1, y_1, 0) \\ &\quad -q_2^2 \sum \hat{w}_{\parallel}(x_2, y_2, x_2, y_2, 0) \\ &\quad -q_1 q_2 \sum \left( \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s) + \hat{w}_{\parallel}(x_2, y_2, x_1, y_1, -s) \right) \end{split}$$

$$+\Delta w_{\parallel \mathbf{r}},$$

and to compare this expression with the field energy calculated from the amplitudes  $\hat{A}$  of the modes. The mode amplitudes excited by both particles are just given by the superposition  $\hat{A} = \hat{A}^{(1)} + \hat{A}^{(2)}$  of  $\hat{A}^{(1)} = -q_1 \hat{v}^*(x_1, y_1)/\sqrt{\hat{W}}$ , excited by  $q_1$ , and  $\hat{A}^{(2)} = -q_2 \hat{v}^*(x_2, y_2)/\sqrt{\hat{W}} \exp(-i\hat{\omega}s)$ , excited by  $q_2$ . Therefore the gain of field energy stored in the oscillating modes is

$$\begin{split} \Delta \mathcal{W}_{\text{EM,modes}} &= \sum \left| q_1 \hat{v}^*(x_1, y_1) + q_2 \hat{v}^*(x_2, y_2) \exp(-\mathrm{i}\,\hat{\omega}s/c) \right|^2 \\ &= q_1^2 \sum |v(x_1, y_1)|^2 \\ &+ q_2^2 \sum |v(x_2, y_2)|^2 \\ &+ 2q_1 q_2 \sum \operatorname{Re} \left\{ \hat{v}^*(x_1, y_1) \hat{v}(x_2, y_2) \exp(\mathrm{i}\,\hat{\omega}s) \right\}. \end{split}$$

Comparing terms of the same mode with the same charges, we get

$$\begin{split} \hat{w}_{\parallel}(x_1, y_1, x_1, y_1, 0) &= -|\hat{v}(x_1, y_1)|^2 = -\hat{k}(x_1, y_1), \\ \hat{w}_{\parallel}(x_2, y_2, x_2, y_2, 0) &= -|\hat{v}(x_2, y_2)|^2 = -\hat{k}(x_2, y_2), \\ \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s) + \hat{w}_{\parallel}(x_2, y_2, x_1, y_1, -s) &= -2\operatorname{Re}\left\{\hat{v}^*(x_1, y_1)\hat{v}(x_2, y_2)\exp(\mathrm{i}\,\hat{\omega}s)\right\}. \end{split}$$

These equations provide information about the per-mode wake functions for any s, without the s > L restriction imposed in Section 3.2; they are derived in Appendix B by another method. In particular, we find that for  $x_1 = x_2$  and  $y_1 = y_2$ ,

$$\hat{w}_{\parallel}(x_1, y_1, x_1, y_1, s) + \hat{w}_{\parallel}(x_1, y_1, x_1, y_1, -s) = -2\hat{k}(x_1, y_1)\cos(\hat{\omega}s/c).$$

It seems natural to claim causality for the individual mode functions, so that we get the *fundamental theorem of beam loading*:

$$\hat{w}_{\parallel}(x_1, y_1, x_1, y_1, s) = -\hat{k}(x_1, y_1) \begin{cases} 0 & \text{for } s < 0, \\ 1 & \text{for } s = 0, \\ 2\cos(\hat{\omega}s/c) & \text{otherwise.} \end{cases}$$

Indeed, in Appendix B it is shown that for closed-cavity volumes,

$$w_{\parallel}(x_1, y_1, x_1, y_1, s > 0) = -2\sum \hat{k}(x_1, y_1)\cos(\hat{\omega}s/c);$$

however, it is also found that the individual mode functions differ from the fundamental beam loading equation for |s| < L. Usually this discrepancy is no problem, as the *short-range* regime of interactions in the same bunch is quite distinct from the *long-range* regime of bunch-to-bunch interactions. The short-range wake is mostly calculated by time-domain methods without any distinction between  $\hat{\omega} \neq 0$  and  $\hat{\omega} = 0$  eigenmodes, whereas the long-range wake is calculated for s > L from oscillating eigenmodes.

Formally the discrepancy can be solved by *definition*: the per-mode wake functions are causal, and the residual wake function is just the difference between the wake function and the summation over the so-defined per-mode functions. In the case of closed cavities, as considered in Appendix B, this leads to a residual wake that is zero.

Thus we come to an interesting consequence of the beam loading theorem: a source particle  $q_1$  loses energy  $q_1V$  with  $V = q_1\hat{k}$ , but a test particle that follows at a very short distance (and with the same offset) observes the voltage -2V.

#### 3.5 Loss parameters

Loss parameters describe the loss of energy of a source particle or source distribution to electromagnetic field energy.

We have seen that the total energy loss of a point particle is given by the wake function for  $x_1 = x_2$ ,  $y_1 = y_2$  and s = 0, so that

$$k_{\text{tot}} = -w(x_1, y_1, x_2, y_2, 0) = \mathcal{W}_{\text{EM,total}}/q_1$$

and we know that the loss to eigenmodes is given by the per-mode loss parameters

$$\hat{k} = |v(x_1, y_1)|^2.$$

The sum of all the per-mode loss parameters converges for cavities *with* beam pipes to a value below the total loss parameter  $k_{tot}$ , as not only are there modes excited, but also field energy is scattered and propagates along the beam pipes. (The wake of a closed cavity is completely determined by oscillating modes, but the sum is divergent.)

The wake potential (of distributed sources) and the shape-dependent loss parameter are usually calculated directly using electromagnetic time-domain solvers. The shape-dependent total loss parameter is the convolution of the longitudinal wake potential with the charge density function; for instance, for bunches with longitudinal profile  $\lambda(z,t) = \lambda(z - ct)$  and negligible transverse dimensions,

$$k_{\text{tot},\sigma} = -\int_{-\infty}^{\infty} W(x_1, y_1, x_1, y_1, z)\lambda(z) \,\mathrm{d}z.$$

The excitation of eigenmodes by distributed sources was discussed in Section 3.2; the shape-dependent per-mode loss parameter for a thin Gaussian bunch is

$$\hat{k}_{\sigma} = \hat{k} \exp\left(-(\hat{\omega}\sigma/c)^2\right),\,$$

and for a general longitudinal profile  $\lambda$  it is

$$\hat{k}_{\sigma} = \hat{k} \left| \int_{-\infty}^{\infty} \lambda(z) \cos(\hat{\omega}z/c) \,\mathrm{d}z \right|^{2}.$$

For closed cavities, the sum of the per-mode loss parameters  $k_{\sigma}$  converges to the total loss parameter  $k_{\text{tot},\sigma}$ . This is also true for long bunches with  $\sigma \gg c/\omega_{\text{cutoff}}$ , which cannot excite frequencies above the lowest cutoff frequency  $\omega_{\text{cutoff}} \propto \pi c/a$  of the beam pipes, where a is the characteristic transverse dimension of the pipes.

For the extreme case of ultra-short bunches it is difficult to calculate the wake potential, as a very high spatial resolution is required. In this case, only a small fraction of energy is lost to resonant modes and only a small part of the wakes is caused by resonances.

#### 3.6 Analytical calculation for a pillbox

For a closed pillbox cavity, all modes can be calculated analytically [21]. Consider a pillbox with radius R and gap length g.

The normalized electromagnetic field of the monopole modes indexed by (n, p) is given by

$$\hat{E}_{z}^{(n,p)} = \frac{j_{n}}{R} J_{0}\left(j_{n} \frac{r}{R}\right) \cos\left(\frac{\pi p z}{g}\right) \exp(\mathrm{i}\,\hat{\omega}_{n,p}\,t),$$
$$\hat{E}_{r}^{(n,p)} = \frac{\pi p}{g} J_{1}\left(j_{n} \frac{r}{R}\right) \sin\left(\frac{\pi p z}{g}\right) \exp(\mathrm{i}\,\hat{\omega}_{n,p}\,t),$$

$$\hat{H}_{\phi}^{(n,p)} = \mathrm{i}\,\hat{\omega}_{n,p}\,\epsilon_0\,J_1\left(j_n\,\frac{r}{R}\right)\,\cos\left(\frac{\pi\,p\,z}{g}\right)\,\exp(\mathrm{i}\,\hat{\omega}_{n,p}\,t),$$

where  $j_n$  is the *n*th zero of the Bessel function  $J_0(x)$  and

$$\left(\frac{\hat{\omega}_{n,p}}{c}\right)^2 = \left(\frac{j_n}{R}\right)^2 + \left(\frac{\pi p}{g}\right)^2.$$

Note that we now write the mode index explicitly as a double index (n, p). The stored energy is given by

$$\hat{\mathcal{W}}_{n,p} = \frac{\mu_0}{2} \int_0^R \mathrm{d}r \, r \int_0^{2\pi} \mathrm{d}\varphi \int_0^g \mathrm{d}z \, \hat{H}_{\varphi}^{(n,p)} \left(\hat{H}_{\varphi}^{(n,p)}\right)^* \\ = \frac{\pi\epsilon_0}{4} \left(\frac{\hat{\omega}_{n,p}}{c}\right)^2 g \, R^2 \, J_1^2(j_n).$$

Hence the normalized voltage on the axis becomes

$$\hat{v}_{n,p} = \frac{1}{2\sqrt{\hat{\mathcal{W}}_{n,p}}} \int_{z}^{g} \mathrm{d}z \, E_{z}(r=0,z,t=z/c)$$
$$= \frac{\mathrm{i}}{\sqrt{\pi\epsilon_{0}g}} \frac{1 - (-1)^{p} \exp(\mathrm{i}\,\hat{\omega}_{n,p}\,g/c)}{j_{n}\,J_{1}(j_{n})},$$

and the loss parameters can now be calculated as

$$\hat{k}_{n,p} = |\hat{v}_{n,p}|^2 = \frac{2}{\pi \epsilon_0 g} \frac{1 - (-1)^p \cos(\hat{\omega}_{n,p} g/c)}{j_n^2 J_1^2(j_n)},$$

so that the expression for the monopole wake function becomes

$$w_{\parallel}(s) = -2\sum_{n=1}^{\infty}\sum_{p=0}^{\infty}\hat{k}_{n,p}\cos(\hat{\omega}_{n,p}\,s/c).$$

The wake function is the sum of all the voltages induced in all the modes.

For a Gaussian bunch with charge density

$$\rho(\mathbf{r},t) = q_1 \,\delta(x)\delta(y)\lambda(z-ct), \qquad \lambda(s) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left(-\frac{s^2}{2\,\sigma^2}\right),$$

the wake potential is given by

$$W_{\parallel}(s) = \int_{-\infty}^{\infty} \lambda(s - s') w_{\parallel}(s') \,\mathrm{d}s'.$$

But even for such a simple example as a pillbox cavity, it is very hard to compute the wake potential by a modal analysis since many modes are needed. The reason is that for *s* inside the bunch, the charge distribution contributing to the wake potential is cut off because of causality. Hence the Fourier spectrum of the charge distribution contains many (say >1000) modes. Since an accelerator is not made up of closed boxes, the modal analysis is not sufficient for calculating the wake potential. The continuous spectrum of waveguide modes in the beam pipes contributes also to the impedance, especially to the short-range wake.

# 4 Impedances

# 4.1 Definitions

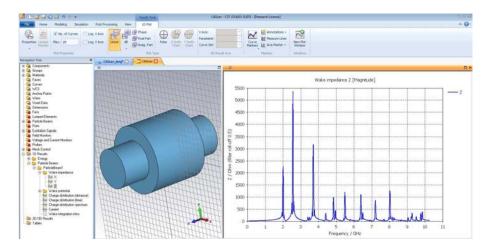
The Fourier transform of the negative<sup>3</sup> wake function is called the impedance or coupling-impedance:

$$Z_{\parallel}(x_1, y_1, x_2, y_2, \omega) = -\frac{1}{c} \int_{-\infty}^{\infty} \mathrm{d}s \, w_{\parallel}(x_1, y_1, x_2, y_2, s) \exp(-\mathrm{i}\,\omega s/c).$$

The wake function and impedance are two descriptions of the same thing, namely the coupling between the beam and its environment. The wake function is the time-domain description, while the impedance is the frequency-domain description:

$$w_{\parallel}(x_1, y_1, x_2, y_2, s) = -\frac{1}{2\pi} \int_{-\infty}^{\infty} \mathrm{d}\omega \, Z_{\parallel}(x_1, y_1, x_2, y_2, \omega) \exp(\mathrm{i}\,\omega s/c).$$

The reason for the usefulness of the impedance is that it often contains a number of sharply defined frequencies corresponding to the modes of the cavity or the long-range part of the wake. Figure 11 shows the real part of the impedance for a cavity. Below the cutoff frequency of the beam pipe, there is a sharp peak for each cavity mode. The spectrum above the cutoff frequency is continuous, caused by residual fields (not related to eigenmodes) and by the 'turn-on' of the harmonic eigen-oscillations. The continuous part of the spectrum is important for short-range wakes, especially for very short bunches.



**Fig. 11:** Real part of the impedance for a cavity with side pipes; the peaks correspond to cavity modes. The results were obtained with the CST wakefield solver.

For the transverse impedance, it is often convenient to use a definition containing an extra factor i:

$$\mathbf{Z}_{\perp}(x_1, y_1, x_2, y_2, \omega) = \frac{\mathrm{i}}{c} \int_{-\infty}^{\infty} \mathrm{d}s \, \boldsymbol{w}_{\perp}(x_1, y_1, x_2, y_2, s) \exp(-\mathrm{i}\,\omega s/c).$$

The reason is that the transverse–longitudinal relations due to the Panofsky–Wenzel theorem then read as follows in the frequency domain:

$$\frac{\omega}{c} \mathbf{Z}_{\perp}(x_1, y_1, x_2, y_2, \omega) = \left( \mathbf{e}_x \frac{\partial}{\partial x_2} + \mathbf{e}_y \frac{\partial}{\partial y_2} \right) Z_{\parallel}(x_1, y_1, x_2, y_2, \omega).$$

<sup>&</sup>lt;sup>3</sup>The sign is chosen so as to obtain a non-negative real part for  $x_1 = x_2$  and  $y_1 = y_2$ .

#### 4.2 Some properties of impedances and wakes

In the spatial s-domain, the relationship between the wake potential of a line charge density  $\lambda(z - ct)$ and the wake functions of a point particle is described by the convolution

$$W(x_1, y_1, x_2, y_2, s) = \int_{-\infty}^{\infty} \mathrm{d}z \, w(x_1, y_1, x_2, y_2, s+z) \lambda(z).$$

The corresponding equation in the frequency domain for the Fourier transform of the negative wake potential is  $V(x_1, y_1, x_2, y_2, \omega) = Z_{\parallel}(x_1, y_1, x_2, y_2, \omega)I(\omega)$ , where

$$I(\omega) = \int_{-\infty}^{\infty} i(t) \exp(-i\omega t) dt = \int_{-\infty}^{\infty} c\lambda(-ct) \exp(-i\omega t) dt$$

is the beam current in the frequency domain. The energy loss of the bunch to electromagnetic fields,

$$\mathcal{W}_{\text{loss}} = \int_{-\infty}^{\infty} W(x_1, y_1, x_1, y_1, s) \lambda(-s) \, \mathrm{d}s$$
  
=  $\frac{1}{2\pi} \int_{-\infty}^{\infty} V(x_1, y_1, x_1, y_1, \omega) I(\omega)^* \, \mathrm{d}\omega$   
=  $\frac{1}{\pi} \int_{0}^{\infty} \operatorname{Re}\{Z(x_1, y_1, x_1, y_1, \omega)\} |I(\omega)|^2 \, \mathrm{d}\omega,$ 

has to be non-negative for any bunch shape  $\lambda$ . Therefore the real part of the longitudinal impedance must be non-negative for all offsets with  $x_1 = x_2$  and  $y_1 = y_2$ . The real part can be negative for, say,  $x_1 = -x_2$  and  $y_1 = -y_2$ , for a structure with azimuthal symmetry and frequency close to a dipole resonance.

As the wake potential is a real function, the real part of the impedance is an even function of the frequency while the imaginary part is an odd function of it:

$$\operatorname{Re}\{Z_{\parallel}(\ldots,\omega)\} = \operatorname{Re}\{Z_{\parallel}(\ldots,-\omega)\}, \qquad \operatorname{Im}\{Z_{\parallel}(\ldots,\omega)\} = -\operatorname{Im}\{Z_{\parallel}(\ldots,-\omega)\}.$$

Hence, the wake function is given in terms of the impedance as

$$w_{\parallel}(\dots,s) = -\frac{1}{2\pi} \int_{-\infty}^{\infty} d\omega \, Z_{\parallel}(\dots,\omega) \exp(\mathrm{i}\,\omega s/c) \\ = -\frac{1}{2\pi} \int_{-\infty}^{\infty} d\omega \, \left( \operatorname{Re}\{Z_{\parallel}(\dots,\omega)\} \cos(\omega s/c) - \operatorname{Im}\{Z_{\parallel}(\dots,\omega)\} \sin(\omega s/c) \right).$$

Furthermore, the electromagnetic field ahead of the source particle is zero for v = c, as electromagnetic waves cannot overtake the source. Therefore, the wake function is *causal*, and the real and imaginary parts of the impedance are dependent on each other. From  $w_{\parallel}(\ldots, s < 0) = 0$  it follows that for u = -s > 0,

$$\int_{-\infty}^{\infty} \mathrm{d}\omega \operatorname{Re}\{Z_{\parallel}(\ldots,\omega)\}\cos(\omega u/c) = -\int_{-\infty}^{\infty} \mathrm{d}\omega \operatorname{Im}\{Z_{\parallel}(\ldots,\omega)\}\sin(\omega u/c),$$

so only the real (or imaginary) part of the impedance is really needed:

$$w_{\parallel}(\ldots,s>0) = \frac{1}{\pi} \int_{-\infty}^{\infty} \mathrm{d}\omega \operatorname{Re}\{Z_{\parallel}(\ldots,\omega)\}\cos(\omega s/c).$$

# 4.3 Shunt impedance and quality factor

The modal part of the wake function is

$$\hat{\boldsymbol{w}}(x_1, y_1, x_2, y_2, s) = -2 \operatorname{Re} \left\{ \hat{v}^*(x_1, y_1) \hat{\boldsymbol{v}}(x_2, y_2) \exp(\mathrm{i}\,\hat{\omega}s/c) \right\} \begin{cases} 0 & \text{for } s < 0, \\ 1 & \text{for } s = 0, \\ 2 & \text{otherwise.} \end{cases}$$

We are interested in the longitudinal component on the axis  $(x_1 = y_1 = x_2 = y_2 = 0)$ , and for simplicity we omit the transverse coordinates, so

$$\hat{w}_{\parallel}(s) = -2\hat{k}\cos(\hat{\omega}s/c) \begin{cases} 0 & \text{for } s < 0, \\ 1 & \text{for } s = 0, \\ 2 & \text{otherwise} \end{cases}$$

Then the impedance per mode,

$$\hat{Z}_{\parallel}(\omega) = -\frac{1}{c} \int_{-\infty}^{\infty} \hat{w}_{\parallel}(s) \exp(-\mathrm{i}\,\omega s/c) \,\mathrm{d}s,$$

is calculated as

$$\hat{Z}_{\parallel}(\omega) = 2\hat{k}\left\{\pi\delta(\omega+\hat{\omega}) + \pi\delta(\omega-\hat{\omega}) + \frac{\mathrm{i}\,\omega}{\hat{\omega}^2 - \omega^2}\right\}.$$

This is equivalent to the impedance of a parallel resonant circuit (see Fig. 12),

$$\hat{Z}_{\parallel}(\omega) = \lim_{\hat{R} \to \infty} \left( i \, \omega \hat{C} + \frac{1}{i \, \omega \hat{L}} + \frac{1}{\hat{R}} \right)^{-1}$$

with  $\hat{C}=1/(2\hat{k}),$   $\hat{L}=2\hat{k}/\hat{\omega}^2$  and  $\hat{R}\rightarrow\infty.$ 

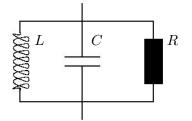


Fig. 12: Equivalent circuit model of the impedance of one mode

Although the resistor  $\hat{R}$  was introduced for obvious formal reasons, it is helpful to consider weak losses of a resonator with a high quality factor  $\hat{Q} = \hat{R}/(\hat{\omega}\hat{L})$ . The impedance per mode of a resonator with weak losses is

$$\hat{Z}_{\parallel}(\omega) = 2\hat{k} \frac{\mathrm{i}\,\omega}{\hat{\omega}^2 - \omega^2 + \mathrm{i}\,\omega\hat{\omega}/\hat{Q}}.$$

The resistor  $R = \hat{Z}_{\parallel}(\hat{\omega}) = 2\hat{k}\hat{Q}/\hat{\omega}$  is called the *shunt impedance*. The *quality factor*  $\hat{Q}$  describes the decay time

$$\hat{\tau} = 2\hat{Q}/\hat{\omega},$$

the resonance bandwidth

$$\Delta \hat{\omega} = \omega / \hat{Q},$$

with  $|\hat{Z}_{\parallel}(\hat{\omega})/\hat{Z}_{\parallel}(\hat{\omega} \pm \Delta \hat{\omega}/2)|^2 \approx 2$ , and the energy loss per unit time

$$\hat{P} = \hat{\omega}\hat{\mathcal{W}}/\hat{Q}.$$

The last relation is used to determine the quality factor by perturbation theory: the energy loss (without beam) is caused by wall losses; as a good approximation these can be calculated from the fields obtained for the mode with infinite conductivity. If  $\hat{H}_t$  is the magnetic field tangential to the surface, the total power dissipated into the wall is given by a surface integral

$$\hat{P} = \frac{1}{2} \int_{\partial V} \operatorname{Re} \left\{ \hat{\boldsymbol{E}}_{s} \times \hat{\boldsymbol{H}}^{*} \right\} \cdot d\boldsymbol{A} = \frac{1}{2} \int_{\partial V} \sqrt{\frac{\hat{\omega}\mu}{2\kappa}} \, |\hat{\boldsymbol{H}}|^{2} \, d\boldsymbol{A}$$

where  $\hat{E}_s = Z_s n \times \hat{H}$  is the tangential component of the electric field on the surface, with surface impedance  $Z_s = \sqrt{i \hat{\omega} \mu / \kappa}$  for conductivity  $\kappa$ .

# Appendix A: Eigenmodes of a closed cavity

We consider a (simply connected) cavity volume  $V_c$ , with perfectly conducting walls (boundary  $\partial V_c$ ) and without current density. We search for time-harmonic eigensolutions, which can be written as

$$E(\mathbf{r}, t) = \hat{E}(\mathbf{r}) \cos(\hat{\omega}t),$$
$$B(\mathbf{r}, t) = \hat{B}(\mathbf{r}) \sin(\hat{\omega}t),$$

where  $\hat{E}$  and  $\hat{B}$  are the eigenfields and  $\hat{\omega}$  the (angular) eigenfrequencies. Substituting these into Maxwell's equations gives

$$abla arepsilon E = \hat{
ho},$$
 $abla imes \hat{E} = -\hat{\omega}\hat{B},$ 
 $abla \hat{B} = 0,$ 
 $abla imes \mu^{-1}\hat{B} = -\hat{\omega}\varepsilon\hat{E}.$ 

We apply the operator  $\nabla \times \mu^{-1}$  to the first curl equation and use the second curl equation to eliminate the magnetic flux density, thus obtaining the eigenproblem

$$\varepsilon^{-1} \nabla \times \mu^{-1} \nabla \times \hat{\boldsymbol{E}} = \hat{\lambda} \hat{\boldsymbol{E}},$$

with the eigenvalues  $\hat{\lambda} = \hat{\omega}^2$  and the boundary condition  $\boldsymbol{n} \times \hat{\boldsymbol{E}} = \boldsymbol{0}$ . The operator  $\varepsilon^{-1} \nabla \times \mu^{-1} \nabla \times$  is self-adjoint<sup>4</sup> with scalar product

$$\langle \boldsymbol{A}, \boldsymbol{B} \rangle = \frac{1}{2} \int_{V_{c}} \varepsilon \boldsymbol{A} \cdot \boldsymbol{B} \, \mathrm{d} V.$$

Therefore the problem has an infinite number of discrete real eigenvalues and a complete orthogonal system of eigenvectors,

$$\langle \boldsymbol{E}_{\xi}, \boldsymbol{E}_{\tau} \rangle = \mathcal{W}_{\xi} \delta_{\xi \tau},$$

where  $\hat{W}_{\xi}$  is the electromagnetic field energy of mode  $\xi$ . The eigenvalues  $\hat{\lambda}$  are non-negative so that all eigenfrequencies  $\hat{\omega}$  are real.<sup>5</sup>

<sup>&</sup>lt;sup>4</sup> The property  $\langle \varepsilon^{-1} \nabla \times \mu^{-1} \nabla \times \mathbf{A}, \mathbf{B} \rangle = \langle \mathbf{A}, \varepsilon^{-1} \nabla \times \mu^{-1} \nabla \times \mathbf{B} \rangle$  can be shown with help of the identity  $\nabla [\mathbf{A} \times \mu^{-1} \nabla \times \mathbf{B} - \mathbf{B} \times \mu^{-1} \nabla \times \mathbf{A}] = \mathbf{B} \times \nabla \times \mu^{-1} \nabla \times \mathbf{A} - \mathbf{A} \times \nabla \times \mu^{-1} \nabla \times \mathbf{B}$  and the divergence theorem. The left-hand side gives a surface integral that is zero because of the boundary conditions. The right-hand side corresponds to the assertion.

<sup>&</sup>lt;sup>5</sup> This property can be shown by using the identity  $\nabla[\hat{E} \times \mu^{-1}\nabla \times \hat{E}] = \mu^{-1}(\nabla \times \hat{E})^2 - \hat{E}\nabla \times \mu^{-1}\nabla \times \hat{E}$  and the divergence theorem. The left-hand side gives a surface integral that is zero because of the boundary conditions. The volume integral of the first term on the right-hand side is non-negative; the integral of the second term gives  $-2\hat{\lambda}\hat{W}$ . As  $\hat{W}$  is positive,  $\hat{\lambda}$  cannot be negative.

There are obviously two types of eigensolutions:

$$\hat{\omega} = 0, \qquad \hat{\omega} \neq 0,$$
  
 $abla \varepsilon \hat{E} \not\equiv 0, \qquad 
abla \varepsilon \hat{E} = 0,$   
 $abla \times \hat{E} = 0, \qquad 
abla \times \hat{E} = -\hat{\omega}\hat{B},$   
 $\hat{B} \equiv 0, \qquad \hat{B} \not\equiv 0.$ 

Eigenfields for  $\hat{\omega} = 0$  are curl-free and are just solutions to the electrostatic problem for any source distribution  $\hat{\rho}$  and the boundary condition  $n \times \hat{E} = 0$ . Oscillating eigenfields are free of divergence; this is a consequence of Maxwell's second curl equation.

In Appendix B we use the property that any linear combination of eigensolutions with  $\hat{\omega} = 0$  is orthogonal to any linear combination of oscillating eigenfields.

## Appendix B: Wake of a closed cavity

We consider a (simply connected) cavity volume  $V_c$  of arbitrary shape, with perfectly conducting walls, that is located between the planes z = 0 and z = L. It is traversed by a point particle with charge  $q_1$ , offset  $(x_1, y_1)$  and velocity v = c. The stimulating charge and current density are

$$\rho(\mathbf{r},t) = q_1 \delta(x - x_1) \delta(y - y_1) \delta(z - ct),$$
  
$$\mathbf{j}(\mathbf{r},t) = c \mathbf{e}_z \rho(\mathbf{r},t).$$

We use the complete orthogonal system of eigensolutions to describe the time-dependent electric field:

$$\boldsymbol{E}(\boldsymbol{r},t) = \sum_{\nu \in C} \hat{a}_{\nu}(t) \hat{\boldsymbol{E}}_{\nu}(\boldsymbol{r}),$$

where  $\nu$  is the mode index, C is the set of all indexes and  $\hat{a}_{\nu}(t)$  are the time-dependent coefficients. As in the main text, we shall write all mode-specific quantities with a hat and omit the index  $\nu$ . We solve Maxwell's equations

$$\nabla \varepsilon \boldsymbol{E} = \rho,$$
  

$$\nabla \times \boldsymbol{E} = -\frac{\partial}{\partial t} \boldsymbol{B},$$
  

$$\nabla \boldsymbol{B} = 0,$$
  

$$\nabla \times \mu^{-1} \boldsymbol{B} = \boldsymbol{J} + \varepsilon \frac{\partial}{\partial t} \boldsymbol{E}$$

by applying the operator  $\varepsilon^{-1} \nabla \times \mu^{-1}$  to the first curl equation and eliminating the magnetic flux density with the help of the second curl equation:

$$\varepsilon^{-1} \nabla \times \mu^{-1} \nabla \times \boldsymbol{E} = -\varepsilon^{-1} \frac{\partial}{\partial t} \boldsymbol{J} - \frac{\partial^2}{\partial t^2} \boldsymbol{E}.$$

By using the modal expansion and the eigenmode equation, we obtain

$$\sum_{\nu \in C} \hat{a}(t) \hat{\omega}^2 \hat{\boldsymbol{E}} = -\varepsilon^{-1} \frac{\partial}{\partial t} \boldsymbol{J} - \frac{\partial^2}{\partial t^2} \sum_{\nu \in C} \hat{a}(t) \hat{\boldsymbol{E}}.$$

This set of scalar equations can be decoupled by applying the operator  $\langle \hat{E}_{\xi}, \cdots \rangle$  to both sides and using the orthogonality condition:

$$\hat{a}_{\xi}(t)\hat{\omega}_{\xi}^{2}\hat{\mathcal{W}}_{\xi} = -\varepsilon^{-1}\frac{\partial}{\partial t}\langle \hat{\boldsymbol{E}}_{\xi}, \boldsymbol{J}\rangle - \frac{\partial^{2}}{\partial t^{2}}\hat{a}_{\xi}(t)\hat{\mathcal{W}}_{\xi}.$$

Finally, we substitute the dirac current density and suppress the index, to arrive at

$$\left(\hat{\omega}^2 + \frac{\partial^2}{\partial t^2}\right)\hat{a}(t) = \frac{-1}{\hat{\mathcal{W}}\varepsilon}\frac{\partial}{\partial t}\langle\hat{\boldsymbol{E}},\boldsymbol{J}\rangle = -\frac{cq_1}{2\hat{\mathcal{W}}}\frac{\partial}{\partial t}\hat{E}(x_1,y_1,ct).$$

This ordinary differential equation can be solved<sup>6</sup> to give

$$\hat{a}(t) = \frac{-q}{\sqrt{\hat{\mathcal{W}}}} \operatorname{Re}\left\{\hat{v}^*(x_1, y_1, ct) \exp(\mathrm{i}\,\hat{\omega}t)\right\}$$

with

$$v(x, y, z) = \frac{1}{2\sqrt{\hat{\mathcal{W}}}} \int_{-\infty}^{z} \hat{E}_{z}(x, y, s) \exp(\mathrm{i}\,\hat{\omega}s/c)\,\mathrm{d}s$$

and

$$\frac{\partial}{\partial z}v(x,y,z) = \frac{1}{2\sqrt{\hat{\mathcal{W}}}}\hat{E}_z(x,y,z)\exp(\mathrm{i}\,\hat{\omega}z/c).$$

The longitudinal wake function is the sum over all modes,

$$w_{\parallel}(x_1, y_1, x_2, y_2, s) = \sum_{\nu \in C} \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s),$$

with the 'per-mode' contributions

$$\begin{split} \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s) &= \frac{1}{q_1} \int_{-\infty}^{\infty} \hat{a} \left(\frac{z+s}{c}\right) \hat{E}_z(x_2, y_2, z) \, \mathrm{d}z \\ &= \frac{-1}{\sqrt{\hat{\mathcal{W}}}} \int_{-\infty}^{\infty} \operatorname{Re} \left\{ \hat{v}^*(x_1, y_1, z+s) \exp\left(\mathrm{i}\,\hat{\omega}\frac{z+s}{c}\right) \right\} \hat{E}_z(x_2, y_2, z) \, \mathrm{d}z \\ &= -2 \operatorname{Re} \left\{ \exp(\mathrm{i}\,\hat{\omega}s/c) \int_{-\infty}^{\infty} \hat{v}^*(x_1, y_1, z+s) \frac{\partial}{\partial z} v(x_2, y_2, z) \, \mathrm{d}z \right\}. \end{split}$$

None of these terms is causal, i.e.  $\hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s < 0) \neq 0$ , but the sum has to be! In the following we use causality to find the simplified representation of the longitudinal wake function

$$w_{\parallel}(x_1, y_1, x_1, y_1, s > 0) = -2\sum_{\hat{\omega} \neq 0} \hat{k}(x_1, y_1) \cos(\hat{\omega}s/c)$$

for  $x_1 = x_2$  and  $y_1 = y_2$ , where  $\hat{k}(x_1, y_1)$  is the longitudinal per-mode loss parameter, as defined in the main text. We therefore split the summation over all modes into the components

$$w_{\parallel d}(x_1, y_1, x_2, y_2, s) = \sum_{\hat{\omega}=0} \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s),$$
$$w_{\parallel c}(x_1, y_1, x_2, y_2, s) = \sum_{\hat{\omega}\neq0} \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s)$$

and use the causality relation

$$w_{\parallel d}(x_1, y_1, x_2, y_2, s < 0) + w_{\parallel c}(x_1, y_1, x_2, y_2, s < 0) = 0$$

together with the anti-symmetry of the non-resonant part,

$$w_{\parallel d}(x_1, y_1, x_2, y_2, s) = -w_{\parallel d}(x_2, y_2, x_1, y_1, -s)$$

<sup>&</sup>lt;sup>6</sup> The causal solution of  $\ddot{a} + \omega^2 a = \dot{b}$  is  $a(t) = \operatorname{Re}\{\int_{-\infty}^t b(\tau) \exp(\mathrm{i}\,\omega(t-\tau))\,\mathrm{d}\tau\}.$ 

proved in (A) below, to eliminate  $w_{\parallel d}$ , yielding

$$w_{\parallel}(x_1, y_1, x_2, y_2, s > 0) = w_{\parallel c}(x_1, y_1, x_2, y_2, s) + w_{\parallel c}(x_2, y_2, x_1, y_1, -s).$$

To get the simplified representation for  $x_1 = x_2$  and  $y_1 = y_2$ , we have to show that the condition

(B) 
$$\hat{w}_{\parallel}(x_1, y_1, x_1, y_1, s) + \hat{w}_{\parallel}(x_1, y_1, x_1, y_1, -s) = -2\hat{k}(x_1, y_1)\cos(\hat{\omega}s/c)$$

is fulfilled for eigenmodes with  $\hat{\omega} \neq 0$ .

We will now prove (A) and (B).

(A) For non-oscillating modes ( $\hat{\omega} = 0$ ), the normalized voltage integrals  $\hat{v}(x, y, z)$  are real and the contribution per mode is

$$\hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s) = -2 \int_{-\infty}^{\infty} \hat{v}(x_1, y_1, z+s) \frac{\partial}{\partial z} \hat{v}(x_2, y_2, z) \, \mathrm{d}z.$$

Therefore the required symmetry is fulfilled:

$$\begin{split} \hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s) &= -2 \int_{-\infty}^{\infty} \hat{v}(x_1, y_1, z+s) \frac{\partial}{\partial z} \hat{v}(x_2, y_2, z) \, \mathrm{d}z \\ &= 2 \int_{-\infty}^{\infty} \hat{v}(x_2, y_2, z) \frac{\partial}{\partial z} \hat{v}(x_1, y_1, z+s) \, \mathrm{d}z \\ &= 2 \int_{-\infty}^{\infty} \hat{v}(x_2, y_2, z-s) \frac{\partial}{\partial z} \hat{v}(x_1, y_1, z) \, \mathrm{d}z = -\hat{w}_{\parallel}(x_2, y_2, x_1, y_1, -s). \end{split}$$

The physical meaning of this symmetry is that the energy transfer from particle 1 to particle 2 (by  $\hat{w}_{\parallel}(x_1, y_1, x_2, y_2, s))$  plus the reverse energy transfer (by  $\hat{w}_{\parallel}(x_2, y_2, x_1, y_1, -s))$  is zero. This is obvious as no energy is left to the non-resonant mode after both particles have departed the volume. The voltage  $\hat{v}(x, y, z)$  is zero for z < 0 before the source  $q_1$  entered the cavity and, as the eigensolution is curl-free, it is zero for  $z \ge L$ . Therefore  $\hat{w}_{\parallel}(\dots, s) = 0$  for |s| > L. Two particles can interact only through non-oscillating modes if they are simultaneously in the cavity at any time.

(B) The normalized voltage integral for oscillating modes ( $\omega \neq 0$ ) does not depend on z after  $q_1$ has left the cavity:

$$v(x, y, z > L) = \frac{1}{2\sqrt{\hat{\mathcal{W}}}} \int_{-\infty}^{L} \hat{E}_z(x, y, s) \exp(\mathrm{i}\,\hat{\omega}s/c)\,\mathrm{d}s = v(x, y).$$

Therefore the following integral relation can be derived:

$$\hat{v}^*(x_1, y_1)\hat{v}(x_2, y_2) = \int_{-\infty}^{\infty} \frac{\partial}{\partial z} \left\{ \hat{v}^*(x_1, y_1, z+s)\hat{v}(x_2, y_2, z) \right\} dz$$
  
= 
$$\int_{-\infty}^{\infty} \hat{v}(\cdots_2, z) \frac{\partial}{\partial z} \hat{v}^*(\cdots_1, z+s) dz + \int_{-\infty}^{\infty} \hat{v}^*(\cdots_1, z+s) \frac{\partial}{\partial z} \hat{v}(\cdots_2, z) dz$$
  
= 
$$\int_{-\infty}^{\infty} \hat{v}(\cdots_2, z-s) \frac{\partial}{\partial z} \hat{v}^*(\cdots_1, z) dz + \int_{-\infty}^{\infty} \hat{v}^*(\cdots_1, z+s) \frac{\partial}{\partial z} \hat{v}(\cdots_2, z) dz.$$

This relation is needed to prove the symmetry:

`

$$\hat{w}(x_1, y_1, x_2, y_2, s)$$

$$= -2 \operatorname{Re} \left\{ \exp(i\hat{\omega}s/c) \int_{-\infty}^{\infty} \hat{v}^*(x_1, y_1, z+s) \frac{\partial}{\partial z} \hat{v}(x_2, y_2, z) \, \mathrm{d}z \right\}$$

$$= -2 \operatorname{Re} \left\{ \exp(\mathrm{i}\,\hat{\omega}s/c) \left[ \hat{v}^*(x_1, y_1) \hat{v}(x_2, y_2) - \int_{-\infty}^{\infty} \hat{v}^*(\cdots_1, z+s) \frac{\partial}{\partial z} \hat{v}(\cdots_2, z) \,\mathrm{d}z \right] \right\}$$
  
=  $-2 \operatorname{Re} \left\{ \exp(\mathrm{i}\,\hat{\omega}s/c) \hat{v}^*(x_1, y_1) \hat{v}(x_2, y_2) \right\} - \hat{w}(x_2, y_2, x_1, y_1, -s).$ 

With  $x_1 = x_2$  and  $y_1 = y_2$ , we find that

$$\hat{w}(x_1, y_1, x_1, y_1, s) + \hat{w}(x_1, y_1, x_1, y_1, -s) = -2\hat{k}(x_1, y_1)\cos(\hat{\omega}s/c),$$

where  $\hat{k}(x_1, y_1) = |\hat{v}(x_1, y_1)|^2$ ; in particular, for the origin,

$$\hat{w}(x_1, y_1, x_1, y_1, 0) = -k(x_1, y_1).$$

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